

Flash Flood Hazard Prediction of Shalatin City, Red Sea Coast, Egypt Utilizing HEC-RAS Model

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ABSTRACT

In terms of flood hazards, Shalatin is the least studied of the six major coastal cities in Egypt's Red Sea Governorate. The current study intends to determine the extent to which Shalatin city is exposed to flood hazard in an attempt to address this research gap. Urban flood modeling proved to be the most effective method. All the layers required for modeling were created in ArcGIS software at the greatest possible resolution using remote sensing products and data obtained during the field investigation. Three potential flood events were modeled as one-dimensional unsteady flow using the most recent version (6.0) of the HEC-RAS programme. To quantify the extent of flooding and water depth, as well as the water velocity and flood hazard, three types of maps were created. In comparison to other cities along Egypt's Red Sea coast, the data reveal that Shalatin appears to be less prone to floods. To safeguard the most susceptible areas, two earthen dykes, each around 2000 metres long, are recommended. The current study is the first to tackle the simulation of an Egyptian city's urban flood at a resolution of up to a single building.

Keywords: Flash flood, HEC-RAS, Modeling, Prediction, Urban floods.

INTRODUCTION

Flooding can have serious impacts on peoples and economy. The immediate impacts may include loss of human life, damage to infrastructure, destruction of or damage to property, and damage to build and natural environments. In the longer term, floods can also cause health problems and financial hardship which last for many years (Lamond *et al.*, 2012). The most notable of the long-lasting impacts are the trauma symptoms caused by the death of the loved ones. In the last decades, the impacts of floods have increased worldwide as unusual weather conditions emerging from climate change are altering the rainfall patterns (Rajkhowa & Sarma 2021). Equally important, though receiving less attention, is that population growth, rapid urbanization, and economic development in flood-prone areas are exacerbating the hazards related to flooding (Hemmati *et al.*, 2020).

Nowadays, flood mapping becomes an integral part of flood management (WMO & GWP 2013). In some countries, the mapping activities are specified by legislations, e. g. the European Union Flood Directives (into force since 2007) requires that all member nations should assess all water courses and coastlines that are at risk from flooding, and draw up flood risk maps showing flood extent as well as assets and individuals at risk in these areas (https://ec.europa.eu/environment/water/flood_risk/, accessed 10 August 2021).

Developing flood hazard and flood risk maps often involves flood inundation modeling (Ali 2018). A model is a simplified representation of the real world using equations or a logical set of operations. The methodologies and techniques used for modeling flood hazards have been developed through more than hundred years of refining and testing. The early formulas, first devised about 1914, were simple statistical ones. Later on, it had been recognized that when statistical analysis is applied to the flood records at a single point, a large sampling error is involved. Thus a new concept evolves whereby data from a wide area are combined to establish generalized relation-

ships applicable anywhere within the area (Benson 1962). The early versions of flood models, particularly the unit hydrograph, were originated in the 1930s. These models were event-based, that produce output only for specific time periods (Wheater 2008). This early approach is still widely used to predict floods (Solomatine & Wagener 2011). It was not until 1960s that the continuous simulation of rainfall runoff processes was made available, thanks to the developments in computing power. The notable example of this second generation of models (now referred to as the conceptual models) is the Stanford Watershed Model. Although continuous in time representation, these models were of the lumped category, in which the parameters are spatially averaged to a single value representing the entire catchment. Models of this type are still at the heart of many operational forecasting systems. The third generation (now termed physically based models) took advantage of the continual increase in computing power and the developments in the field of geographic information systems (GIS) in the 1970s and 1980s. These are distributed models in which the model parameters vary spatially. As the recent developments have resulted in more complex data intensive models, the low-complexity floodplain mapping techniques are now promising alternatives (Diehl *et al.*, 2021).

Notwithstanding all these developments, almost all modeling tools have been developed for humid area applications, while arid and semi-arid areas have received little attention (Wheater 2008). Moreover, many well developed methods may have little relevance to developing countries due to the lack of data. Therefore, the availability of data and the context of the study area are important considerations when modeling flood hazards (Dewan 2013). To fill the present data gaps, developing countries can rely on crowdsourcing using low-cost sensors for obtaining observations of hydrometeorological variables. However, due to their relatively low reliability, crowdsourced observations have not been widely integrated into flood forecasting models. Instead, they



have been used to validate model results against observations (Mazzoleni 2016).

As vast expanses on the globe, including deserts and polar regions, are still suffering from the lack of ground-based measurements of hydrometeorological variables, remote sensing (RS) becomes instrumental in providing flood modelers with essential inputs required in addressing this challenge (Mujumdar and Kumar 2013). Additionally, the fact that a lot of the RS products are freely available data indicates the potential that such technology can be extended to developing countries that have not previously been able to benefit from flood predictions (Di Baldassarre 2013).

The case of the deserts of Egypt is an example of the complete lack of runoff data. It is striking to note that, apart from the River Nile proper, all other catchments that cover more than 500,000 km² of the desert area are ungauged. These catchments were scenes of infrequent flash floods. For centuries, the floods went unnoticed as the area most prone to flooding remained sparsely populated. With the increase of population pressure in the Egyptian heartland, a tendency toward developing the periphery had begun since 1970s. As Hermas *et al.*, (2021) point out, the low relief areas of the alluvial fans, wadi beds, and piedmonts represent the most favorable sites for urban development, albeit they are at the outlets of drainage basins.

The cities and infrastructures on the Red Sea coasts were scenes of the salient impacts of the recent destructive floods. A notable case is that of Wadi Abu Had in which the flood during October 2016 had resulted in tens of fatalities and widespread destruction to roads and homes in Ras Gharib city (Elnazer *et al.*, 2017). Nowadays, the flood hazard to the Red Sea cities is recognized as the most significant natural hazard in terms of fatalities and economic damage.

The flood hazards to five of the six main urban centers on the coast of Red Sea Governorate have been subjects of several studies; Ras Gharib (Yehia *et al.*, 2000a; Elnazer *et al.*, 2017 and Hermas *et al.*, 2021), Hurghada and environs (Yehia *et al.*, 2000a; Abd-Elhamid *et al.*, 2018; Abdrabo *et al.*, 2020 and Bauer *et al.*, 2020), Safaga (Yehia *et al.*, 2000b and Masoud 2004), Quseir (Yehia *et al.*, 2000b; Mashaly & Ghoneim 2018), Marsa Alam (Yehia *et al.*, 2000b and Foody *et al.*, 2004). To date, the flood hazard to Shalatin city is still a research gap (Fig. 1).

Another gap of research is that the published studies about the flood hazards to any Egyptian city are limited in scope to the hydrologic models. None of them contains a hydraulic model describing the flood behavior at any scale used in urban flood modeling. The only exception is the contribution made by Mashaly & Ghoneim (2018) for the city of Quseir. However, its major limitation was that it depended exclusively on remotely sensed data without paying visit to the scene, and thus the maps depicting the results were too generalized to be described as urban floods model outputs.

The current study intends to address these two research gaps by answering two questions: To what extent

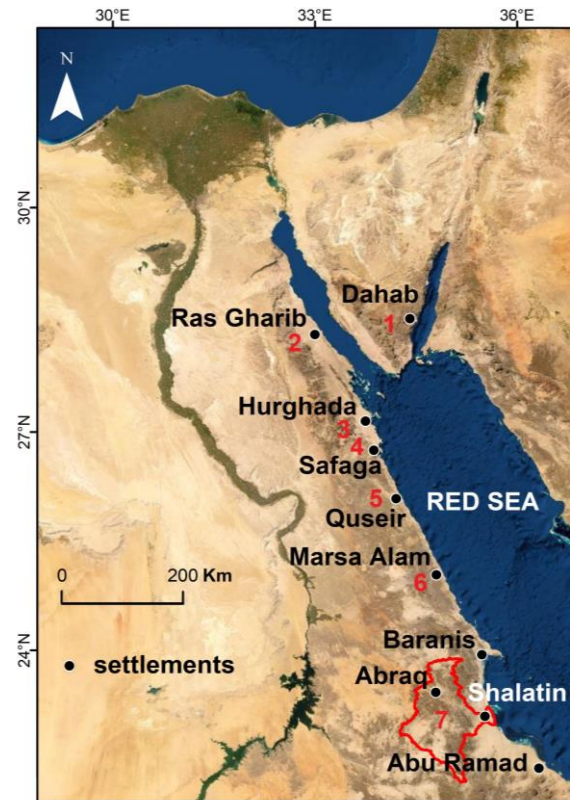


Figure (1): The Red Sea coasts of Egypt and their hinterland. Settlements are shown. The wadis (red number) are dry valleys: 1, Wadi Dahab; 2, Wadi Abu Had; 3, Wadi Umm Sidr; 4, Wadi El Baroud; 5, Wadi El-Ambagi; 6, Wadi El-Alam; 7, Wadi Hudein (with a defined catchment area).

is Shalatin city vulnerable to flood hazard? And what mitigation strategies can be suggested? The easiest way to get the answers is to utilize a hydraulic model in a GIS context to identify the areas of Shalatin that are most vulnerable to flash floods and estimate the related hazard degrees. The current study is the first to use data from remote sensing and field studies to simulate urban floods with a resolution of up to single structures. It's also the first time an Egyptian city's urban flood has been simulated at this fine resolution.

MATERIALS AND METHODS

Study area characteristics

Located between 23° 06' and 23° 09' North and 35° 33' and 35° 37' East, Shalatin (variously transliterated as Shalateen or Al Shalateen) is the southernmost urban center on the Red Sea coast of Egypt, with almost 11,400 inhabitants according to the census of 2017, and an estimated population of 12,000 in 2021. Its built-up area is slightly less than 8 km². The city is accessible through the main highway running alongside the coast, and is linked to Aswan in the Nile Valley through a paved road across the desert. In the aftermath of the so-called Third Halayeb Crisis in 1993, the Egyptian Government started a comprehensive plan to develop the long neglected south eastern part of Egypt. The plan envisaged, inter alia, the promotion of the then small settlement of Shalatin into a full-fledged urban center. Today, the economic base of the city is diversified, and depends on its administrative function,

its unique camel market, as well as its role as service provider located on the main highway linking Egypt and Sudan. It also acts as service provider to the vast hinterland that extends as far as Abraq (westwards) and Abu Ramad (southwards) (personal communications in field study). So far, there are no studies available on the demography and economy of the city).

The location of the original settlement of Shalatin was chosen, by the local tribal groups, to be atop the fan of Wadi Hudein (variously transliterated as Hodein, Hudain or Hudin). Their intention was to reside as near as possible to Shalatin Wells, located in the midst of the course of the main channel that cuts through the fan. For centuries, these wells were a watering spot for camels and goats, thanks to the shallow water table created by infiltration of the waters of infrequent flash floods. These floods result from the draining of the vast (11,850 km²) Hudein Basin (Fig. 2).

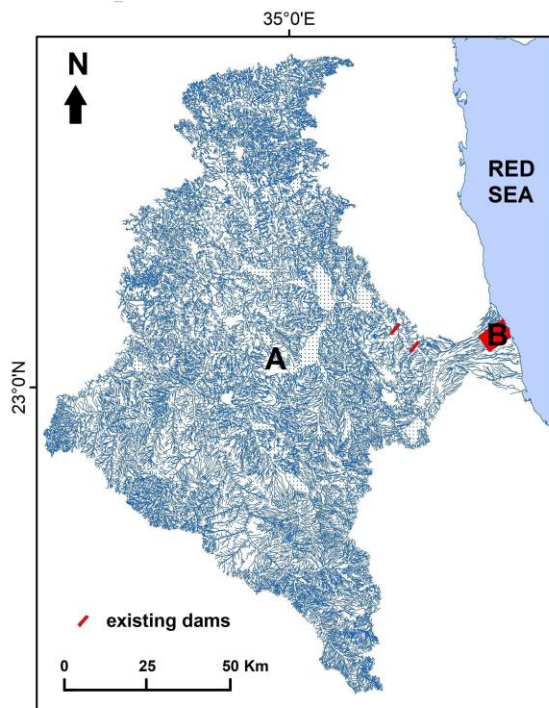


Figure (2): Location map of the study area, A, Wadi Hudein catchment; B, the study area.

The decision to locate the planned new quarters to be close to the main channel and the shore is taken by the government (Fig. 3). During the preparation of the city master plan, two alternatives were considered: planning a city with a maritime façade and tourism as the main economic base, and extending the then existing settlement. The final decision was to adopt the second alternative as it was found that the salt water, rising by capillarity, would severely damage the buildings and infrastructure (General Organization for Physical Planning 1995), and the plan called for "restricting the built up area between 10 and 30 m contour lines.

A characteristic synoptic feature of autumn in the study area is convective storms resulting from the northward incursion of the Active Red Sea Trough triggered by the upper level trough (De Vries *et al.*, 2013 and Morsy *et al.*, 2020). As most of the Hudein

Basin is covered by impervious basement rocks (Ghanem 1972, Shabana *et al.*, 2003 and Sadek 2009), a considerable quantity of rainfall would create runoff. Additionally, the achievement of two "dams" on the main course of the wadi in 2019 puts the city at risk of flooding than ever before, if one of the dams suddenly fails.

Studying the flooding event

The urban flooding simulations are now the main tool that can give insights about flood hazards and risks (Eldho *et al.*, 2018). To simulate an urban flooding event, two models may be constructed: 1. hydrologic model that translates rainfall (at the catchment scale) into stormwater runoff after considering various losses, and, 2. hydraulic model that evaluates the transfer of stormwater flows through networks of infrastructure and across land surfaces. Typically, the input to the second model is the flow amount which is the output of the first model, and the main outputs of the second are the flow extent, the flow height, velocity, and degree of hazard. The simulations can be performed at different spatial scales, of which the smallest is that of a single small parcel of land with a single dwelling. At the other end of the spectrum of scale, the simulation may cover an entire suburb or even a small city (Coombes and Roso 2019). However, the representation of urban micro-features is critical to the accuracy of modeling results (Wang *et al.*, 2018).

Flash floods occur as a result of the higher rate of precipitation than the infiltration rate, supported by increased land slopes. Another cause of flash flood is the collapse of dams and barriers (Fathy *et al.*, 2020). Accordingly, the simulation of floods requires precipitation and/or overland flow data, topographic data, lithology and/or soil data, land use/land cover (LULC) map, the selection of a hydraulic model, geometric data as specified by the model.

Hydrometeorological data

The discharge hydrographs, for certain recurrence periods of 25, 50 and 100 years, can be constructed based on either flood data or rainfall data (Ball and Babister 2019). The efforts to quantify flash flood hazards in drylands are often hampered by the lack of data relevant to the overland flow. Faced by this state-of-affair, modelers usually use the morphometric parameters of the basin to estimate discharge hydrographs (Ghoneim *et al.*, 2002, for Wadi El-Alam; Masoud 2004, for Wadi El Baroud and Omran *et al.*, 2011, for Wadi Dahab). Additionally, Some researchers have devised novel approaches, of which the notables are: a, monitoring the increase in spectral reflectance (due to the deposition of fine sediments) of channels affected by a recent flash flood (El Bastawesy *et al.*, 2009, for Wadi Hudein); and b, field measurements of recent flood debris (Abbas *et al.*, 2020, for Wadi Umm Sidr).

The use of meteorological data to produce hydrographs is an alternative method that is likewise troublesome. Gheith and Sultan (2002) discovered that only four recording stations out of 13 in and around

their study region were equipped and in working order to give valid hyetograph records in a study of the 1994 flooding episodes in the Eastern Desert. The available rainfall data for this study could not meet the minimum requirements because the Shalatin meteorological station was only established on January 1, 2001, and the nearest two meteorological stations (located in Baranis Air Force Base and Qusseir, respectively) are

95 and 350 kilometres away from Shalatin. Additionally, and most strikingly, there are no meteorological stations in the vast hilly country lying between the Red Sea coast and the Nile Valley. This fact led the compilers of the Climatic Atlas of Egypt (EMA 1996) to admit that “the situation in the Eastern Desert is rather difficult because there are no stations established over the chain of the Red Sea mountains”.

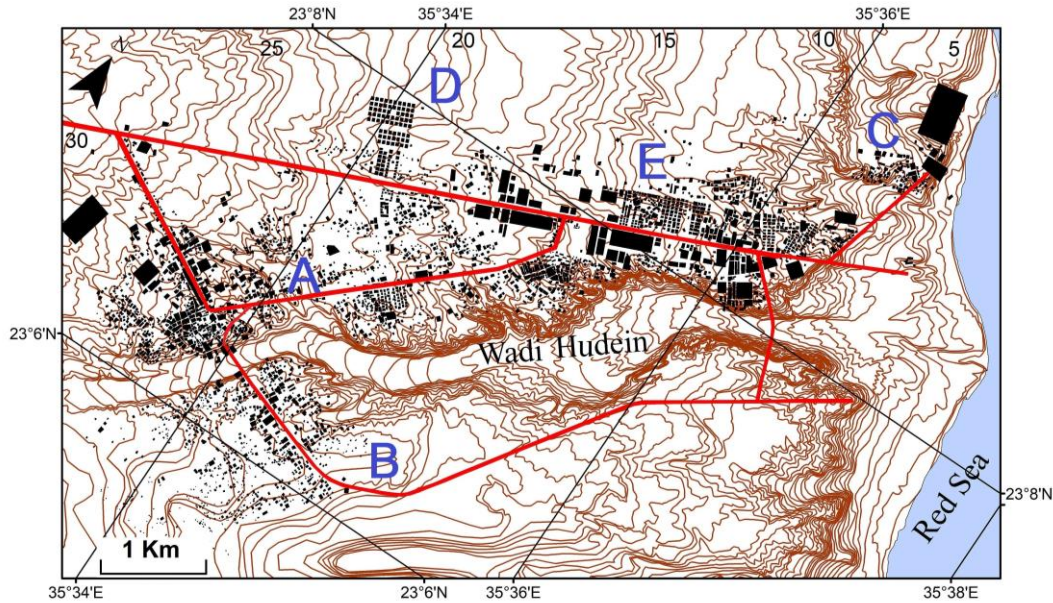


Figure (3): Shalatin's layout (December 2020) displays brown contours with a 0.5-meter interval; black built-up areas; unplanned settlements (A, B, and C) are in the southwest and near the shore (C, fishermen village); the planned model quarters are in the middle (D and E).

The two long-time series of rainfall available for Qusseir (1927 onwards) and Baranis (1964 onwards) (Physical Department 1938, Meteorological Department 1950, Meteorological Authority 1979 and EMA 2011) give maximum rainfall in one day as high as 34 mm in Qusseir (recorded on 6 November 1934) and 48.0 mm and 68.2 mm in Baranis (recorded on 20 October 1979 and 6 May 1976 respectively). The effects of the future climate changes on precipitation cannot be anticipated, as the results obtained from various future climate models seem to be contradictory.

The remotely sensed precipitation data cannot be used to compensate for the lack in the rainfall data. In a comprehensive evaluation of the performance of the three globally high-resolution remotely sensed rainfall products for the Middle East, it was found that all products perform poorly in reproducing the anomalous wet events (El Kenawy *et al.*, 2019). Suffice here is to show the cumulative rainfall in Wadi Hudem basin for the ten days (1 to 10 Nov. 2020) that witnessed 11 mm of rainfall in Shalatin station (as reported by the Egyptian Meteorological Authority). Figure 4 was constructed by converting precipitation data from a netCDF file into a raster dataset with one tenth degree of geographic resolution, then classifying the raster using ArcGIS 10.3 software.

The data are from the Global Precipitation Measurement Mission's (GPM) Final Run version of the product GPM 3IMER-GDF v06, and are publicly

available at the National Aeronautics and Space Administration's (NASA) site:

“<https://giovanni.gsfc.nasa.gov/giovanni/>”.

A consequence of the lack of the adequate meteorological data for the Eastern Desert is the lack of statistical studies addressing the extreme rainfall events for up to 100 years recurrence periods. Indeed, the study of Gado (2020) was the first in this respect, though it is limited southwards to Qusseir. Faced by the lack of data, the present study considered the results of studies of the comparable case of Wadi El-Alam (peak discharge 1,130 m³/s, Ghoneim *et al.*, 2002), and thus the hypothetical discharge hydrographs were assumed to be of a single peak, with peak discharge rates of 500, 1,000 and 1,500 m³/s. These are a rather conservative estimates (to represent 25-100 years recurrence periods) if compared to a peak discharge of 875 m³/s for Wadi El-Ambagi that drains a catchment area of only 1,540 km² (Mashaly & Ghoneim 2018).

The peak discharge of 18,300 m³/s estimated by Elewa *et al.*, (2020) should be regarded as over-estimation, and is not considered here. Adopting hypothetical values for peak discharge eliminates the need for a hydrological model, and all that needed is the hydraulic one, in which the hydrographs are located at a cross section of the wadi lying just on the outskirts of the city, i.e. at 9.6 km from the outlet of the wadi into the Red Sea.

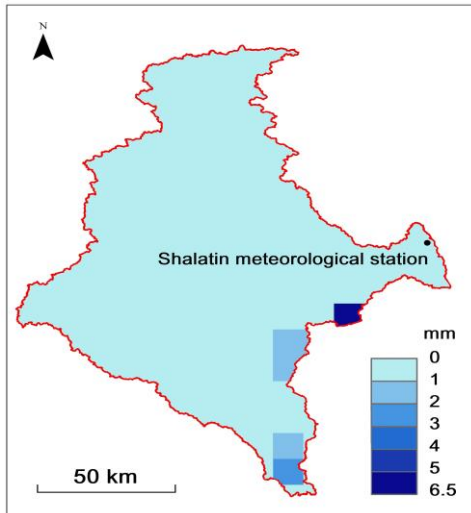


Figure (4): The cumulative rainfall in Wadi-Hudein basin, as acquired by GPM, for the ten rainy days of 1 to 10 November 2020. The dataset gives a remotely sensed value of less than 1 mm for the pixel containing Shalatin meteorological station, and under-estimates the observed value of 11 mm.

Topographic data

Urban flood modeling requires a digital elevation model (DEM) of finer resolution than that of the freely available DEMs. The required resolution should capture the flood behavior at the street or the individual building level. Fortunately, the study area has recently been covered by contour map produced out of aerial photos (Military Survey Authority, 2003). The map is of 0.5 m contour interval. To convert the contours to a raster DEM (Fig. 5A) to be input later in the modeling software, the contours were first digitized as a shapefile layer in ArcGIS 10.3 software, and then interpolated using the Topo to Raster tool. The output DEM cell size was set as 2 m.

The LULC map

The use of such a map is required for the assessment of environmental impacts (Arnous *et al.*, 2017). In urban modeling the need of LULC is of threefold: (1) to convert the DEM to digital surface model (DSM), i.e. to add the footprints of buildings (Wang *et al.*, 2018); (2) to be used, along with the soil texture map, to assign the Manning's n-values to each LULC category. The n-values express the roughness of the terrain and thus are parameters of any flood model; (3) to be used as a layer, among other layers of the results, in the visualization of the flood behavior, either as animation or still maps.

To produce a LULC map capable of satisfying these functions, a satellite image of ArcGIS World Imagery, up to one meter resolution, was used to create shapefiles in ArcGIS. The visual interpretation of these remotely sensed data (Fig. 5C) is based on a comprehensive survey of the urban features during field study of the city in 2018. Four main types of buildings can be recognized (Fig. 6). The sparsely distributed vegetation was extracted using imageries taken in October 2018 and verified in the field (Fig. 7). May, October and November are the months with high rainfall, and consequently flood probability, in southeastern Egypt (Table 1).

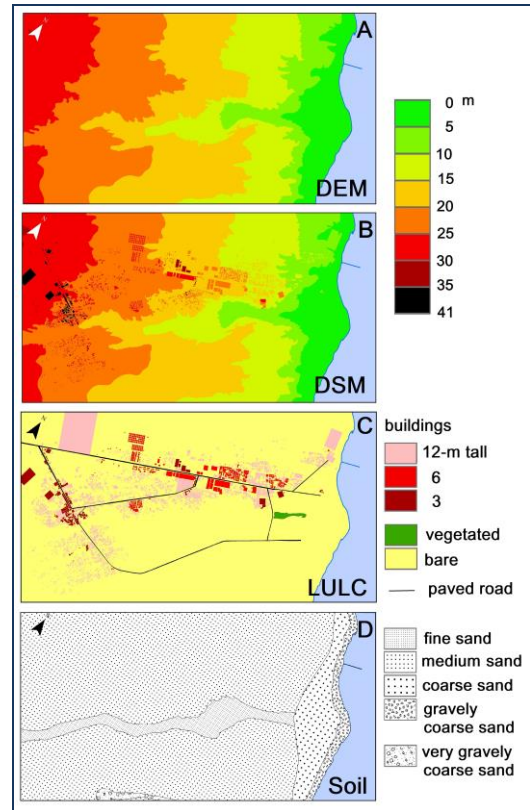


Figure (5): Four layers to be input in the model: A, DEM; B, DSM; C, LULC; D, soil texture



Figure (6): Examples of the four primary building types found in Shalatin. a) in unplanned quarters, fishermen's shanties; b) in planned quarters, bedouin sedentarization houses; c) in planned quarters, one floor; d) in planned quarters, four floors.



Figure (7): The vegetation in the Wadi Hudein bed, in the vicinity of the Shalatin Wells.

The DSM

The DSM (Fig. 5B) is created using the raster calculator tool in of ArcGIS software. The DSM is simply the algebraic sum of two layers; the DEM and the buildings footprints as classified in the LULC map.

The Soil texture map

This map is required by the model to assign Manning's value to each texture category. The map (Fig. 5d) was constructed based on the survey results of representative forty two soil profiles, reported in El-

Taweel and Kotb (2006). The Manning's Roughness Coefficients (n) and the adjustment factors for irregularity (n_1), variation in channel cross section (n_2), obstructions (n_3) and vegetation (n_4), were taken from the guide adopted by the United States Geological Survey (Arcement & Schneider, 1989).

The selected model

The latest version (6.0, launched in December 2020) of HEC-RAS software was used. This package was produced by Hydrologic Engineering Center of the US Army Corps of Engineers, and is freely available at Hydrologic Engineering Center's River Analysis System (HEC-RAS) website (<https://www.hec.usace.army.mil/software/hec-ras/>). HEC-RAS allows the user to perform, among other things, one-dimensional steady flow, and one and two-dimensional unsteady flow simulations (Brunner 2021).

Modeling the case study is better achieved using the one-dimensional unsteady flow option in HEC-RAS (for comparisons of the advantages, disadvantages and the computational details of 1D, 2D and 3D in HEC RAS, see Brunner *et al.*, 2020). The 1D option assumes that the forces acting on a body of water are predominantly along the river channel centerline (x -direction) and that the lateral forces (y -direction) and the vertical (z -direction) are negligible. The simulation results are displayed using the HEC-RAS Mapper module (Brunner 2020), which allows users to view inundation area, water depth, and water velocity as animated or static maps. In the Mapper module, users can also generate their own customized maps and animations. For instance, a flood hazard map can be created by multiplying the water depth layer by the water velocity layer using the raster calculator.

The Geometric data

Hydraulic models require the creation of "Geometry," of which only four are required in this study: "Centerline," which is the channel's centerline, "Banks," which are the channel's two banks, "Path," which is the flood plain's limit or the area prone to inundation, and "Cross Section," which are sections perpendicular to the channel and extending to the Path's limits. The geometries were digitized using the background layer ArcGIS World Imagery in the HEC-RAS Mapper module, and a total of ten cross sections were created, each around one kilometre apart (Fig. 8). Meanwhile, a flowchart summarizes the methods employed (Fig. 9).

RESULTS AND DISCUSSION

The model was run thrice to simulate three events of peak discharges of 500, 1,000 and 1,500 m^3/s . The results of the simulations are visualized in RAS Mapper as animations. Since the hypothetical discharge hydrographs are of 24 hours duration, and as the model was set so that the calculations are performed iteratively at 1 minute interval, a total of 1441 still maps can be obtained for any of the characteristics of the flood. To summarize, the study's goals are to

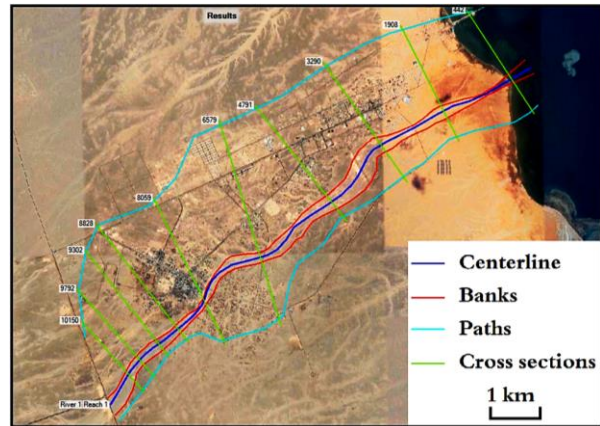


Figure (8): The geometric data required by the model.

visualize three maps: water depth, water velocity, and hazard (Depth X Velocity). The maps that illustrate the worst case scenario in terms of hazard maps were chosen for presentation here from among the numerous available. The worst scenario occurs 13 hours 15 minutes after the commencement of the flood in two events (1,000 and 1,500 m^3/s), and 9 hours 10 minutes after the onset in the 500 m^3/s instance. Figures (10), (11) and (12) illustrate the scenario at these points in time.

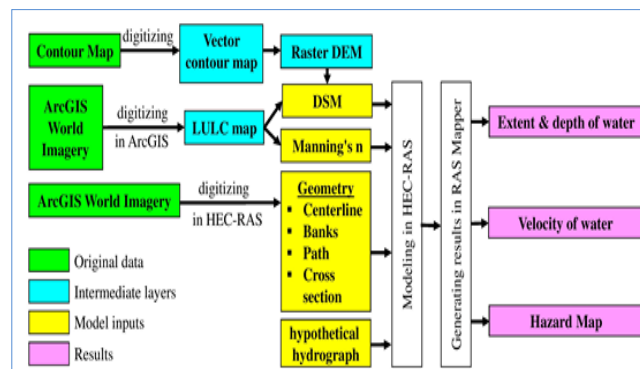


Figure (9): Flowchart of the methodology used.

The results show that, even with the conservative estimation of 500 m^3/s peak discharge, a water depth as high as 1.5 m would build up at the most vulnerable areas, all of which belong to the unplanned quarters (officially categorized as squatted settlements). The city master plan (General Organization for Physical Planning 1995) calls for using the channel only as conduit for flood waters; however, the locals are repeatedly encroaching the channel, but they always face counter reactions taken by the authorities (Fig. 13).

The simulation results for the 1,000 m^3/s peak discharge event show a higher water depth (3 m), localized mainly in the channel, and a depth of 1 to 1.5m at the most vulnerable areas. The hazard of inundation, (Fig.11a), is further aggravated by the relatively high velocity of water (Fig. 11b), and this is why Fig. (11c) shows that tens of homes located near the channel are highly vulnerable. The results demonstrate no substantial divergence from the 1,000 m^3/s simulation for the extreme situation of a 1,500 m^3/s peak discharge, represented in Figure (12).

Table (1): Average and maximum rainfall (mm) in one day for Baranis (Ras Banas) station (1976-2005, EMA, 2011).

Rainfall	Month									
	Jan.	Feb.	Mar.	Apr.	May	Jun. to Sept	Oct.	Nov.	Dec.	
Average	2.9	0.2	1.5	3.7	21.9	0	13.2	11.7	0	
Max	5.5	0.2	2.8	12	68.2	0	48	20	0	

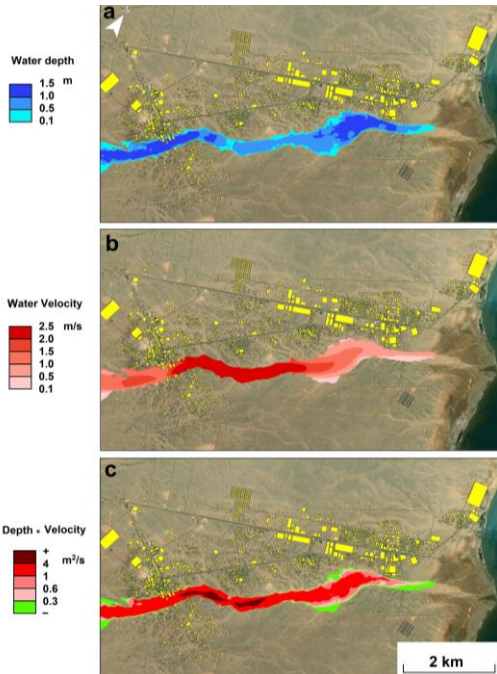


Figure (10): The outcomes of the worst case simulation of a 500 m³/s peak discharge event.

The fisherman villages, as well as certain public buildings in the planned quarters, are now at risk of flooding. In all scenarios, the most vulnerable areas are almost the same.

The building materials in these areas are predominantly wood, along with torn metal pieces and plastics. In some cases limestone is used, but without safety requirements. Such buildings cannot withstand heavy floods. Among the Red Sea coastal cities, Shalatin is unique in preserving this type of shanty houses. The only comparable case is that of the small settlement of Halayeb, located about 165 km SE of Shalatin. Halayeb was given a city status in 2014 albeit being a mere shanty town of wood houses. Highly vulnerable to flooding, almost all Halayeb houses had been swept away or collapsed during the flooding disaster in November 2019.

The present model predictions fit well with the few known observations in comparable cases. In interviews with the Safagan people, Masoud (2004) reported 4 m water level in some parts of the city, and a 2 m water depth has been reported in Quseir during the 1994 and 1996 flash floods (Mashaly & Ghoneim 2018). A similar depth of 2 m was reported in Ras Gharib in 2016 (El Nazer *et al.*, 2017). However, due to the topography of Shalatin, the predicted water depth would be restricted in space, i. e. in the main channel and slightly beyond it. Thus, Shalatin seems to be less vulnerable to floods if compared to Ras Gharib which

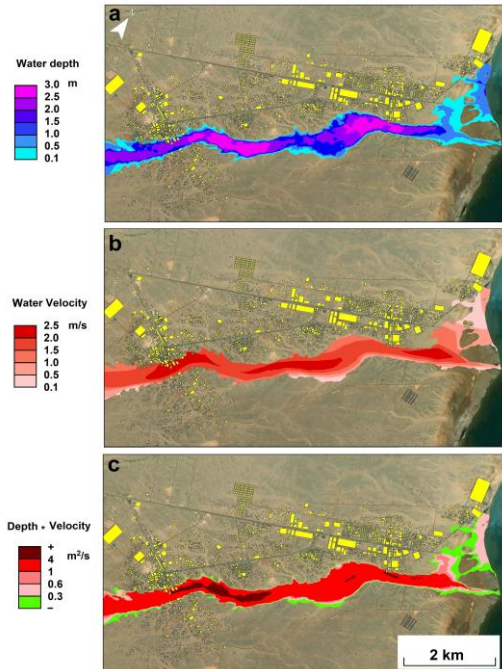


Figure (11): The outcomes of the worst case simulation of a 1,000 m³/s peak discharge event.

was almost totally inundated for six hours in the 2016 events. Also, the area prone to flooding in Shalatin is less than that predicted for Quseir according to the results of the model in Mashaly and Ghoneim (2018).

The interpretation of the three hazard maps (Figs. 10C, 11C and 12C) can be done using the Flood Hazard Vulnerability Curves, devised by Australia Water Research Laboratory (Smith *et al.*, 2014). These curves (reproduced here as Fig. 14) have been measured in controlled tests and after extensive literature review. The five categories depicted in Figs. (11c), and (12c) correspond to the six categories depicted in Fig. 14, with H₂ and H₃ lumped together for convenience. The important result that can be deduced is that not only peoples and vehicles would be at high vulnerability, but even buildings would be vulnerable as well.

A limitation of the present study is that the calibration of the model cannot be achieved using remotely sensed data, as these data are not available for the very time of the known flood events. Calibration may not be possible even for further well-planned studies in the future, as the main channel upstream Shalatin had been dammed. This limitation of study is not specific to the Shalatin case. As Coombes and Roso (2019) put it as the opportunity for inundation model calibration for drylands is very limited and even is practically nonexistent. However, HEC-RAS predictions for different contexts have been proved to

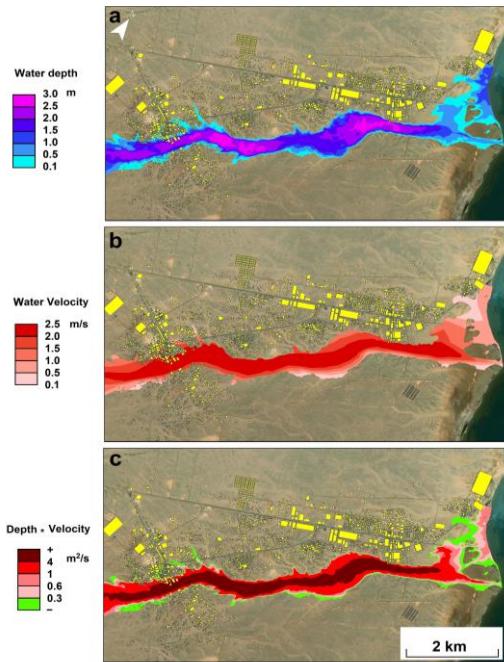


Figure (12): The outcomes of the worst case simulation of a 1,500 m³/s peak discharge event.



Figure (13): Illegal sprawls located in the bottom of Wadi Hudein channel, and demolished by the authorities.

fit welwith the observations. Today HEC-RAS model is one of the most commonly utilized flood modeling pieces of software in hydrodynamic simulation (Dasallas *et al.*, 2019).

One of the implications for future research is that relying only on remotely sensed may prove to be a flawed approach. In a final report about the hazards of floods of Wadi Hudein (NARSS 1997) the investigators ranked the hazard as low. They ground their argumentation on theoretical bases, referring only to the topography of the watershed. In a later study on the wadi, El Bastawesy *et al.*, (2009) concluded that runoff would be lost in transmission into the underlying alluvium before reaching the outlet at the coast. These views were challenged when, in November 2020, a year only following the damming of the main course, a long lake was formed as a consequence of a flood event. The two earthen dykes, achieved in 2019, dam the main course, giving rise to two retention basins, with total storage capacity of 16 million m³.

The work involved 5.4 million m³ of cut and 3.6 million m³ of fill. Paradoxically, the dykes that are intended to mitigate flash floods are themselves a new possible cause for more destructive floods, if one of them fails. Dam failure possibilities were never addressed in research though score of dams have been

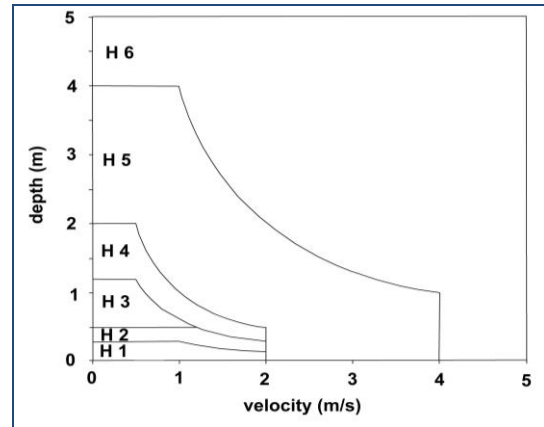


Figure (14): Flood Hazard Vulnerability Curves (after Smith *et al.*, 2014). H1: safe for peoples, vehicles and buildings, H2: unsafe for small vehicles, H3: unsafe for vehicles, children and elderly, H4: unsafe for peoples and vehicles, H5: unsafe for peoples and vehicles, buildings require special design, H6: All building types are vulnerable to failure.

constructed on the main wadis in Egyptian deserts in the last two decades. To date, the only reported case of failure is that of Wadi Dahab dam in 2012 (Abdel-Fattah *et al.*, 2015).

The construction of the two dykes would not guarantee the protection against possible severe flooding. Recommendations - in the light of the newly created situation include: (1) protecting the most vulnerable areas through the construction of two earthen dykes, each about 2000 m long, on both sides of the main channel. This may prove a temporary solution as the housing programs to eradicate the slums were shelved, (2) Initiating a research project to study all possible consequences of the failure of one of the dams, and the worst case of the successive failures of the two. The proposed project may be expanded to include other cases of Red Sea coastal cities.

CONCLUSION

In comparison to other settlements along the Egyptian Red Sea coast, Shalatin appears to be less vulnerable to floods, at least according to modeling data. Even with the lowest forecasts of peak discharge, however, some portions of the city could be flooded. The majority of the homes in these locations are made of wood and are therefore vulnerable. Because plans to rebuild the unplanned quarters beyond the vulnerable areas have been delayed, immediate mitigation measures should be performed, the most practical of which appears to be the wadi embankment within the built-up area. The city has not been effectively safeguarded by the construction of two dykes to dam the major channel. A heavy flood could force the dykes to fail. This evolving nature of flooding hazards puts the city in risk more than ever before, and future study should take this into account. The findings of this study are broadly applicable to various settlements along Egypt's Red Sea coast, as they share many commonalities in terms of local geography, land use/land cover, and the nature and severity of hazards.

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التنبؤ بخطر السيول على مدينة شلاتين، ساحل البحر الأحمر، مصر باستخدام نموذج HEC-RAS

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الملخص العربي

تعد شلاتين أقل المدن الساحلية الست الرئيسية في محافظة البحر الأحمر المصرية من حيث نصيبها من دراسة خطر السيول. وهذه الدراسة محاولة لاستكشاف هذه المنطقة والإجابة عن مدى كون المدينة عرضة للخطر الناتج عن السيول. وقد أجريت محاكاة لخطر السيول الحضري باستخدام لمخرجات الاستشعار من بعد ونتائج الدراسة الميدانية. واستخدم برنامج ArcGIS لإنتاج الطبقات اللازمة كمدخلات للمحاكاة بأكبر درجة ممكنة من التفصيل المكاني. واستخدمت أحدث نسخة من برنامج سلاح المهندسين الأمريكي HEC-RAS لنمذجة ثلاثة أحداث سيول افتراضية كجريان غير ثابت أحادي البعد، بهدف إنتاج ثلاثة أنواع من الخرائط، توضح المساحات التي ستغطيها مياه السيول وعمق الماء، سرعة الماء، خطر السيل معبرا عنه بشكل كمي. وقد أظهرت النتائج أن شلاتين تبدو أقل عرضة لخطر الفيضان مقارنة بنظيراتها من مدن ساحل البحر الأحمر المصري. وتوصي الدراسة ببناء حاجزين ترابييين طول كل منهما نحو 2000 متر على جانبي المجرى الرئيس للوادي لحماية المناطق الأكثر عرضة للخطر. وهذه أول دراسة عن محاكاة السيول الحضرية لأية مدينة مصرية بمستوى تفصيل يصل إلى المبنى المنفرد.